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- The most popular method of initialization up to recently was nonlinear normal mode initialization, or NNMI.
- This has been widely used, in many NWP centres, and has performed satisfactorily.
- However, it has a number of limitations. In particular, it is not straightforward to apply NNMI in limited geographical domains.
- Recently, an alternative method of initialization, called digital filter initialization (DFI), was introduced.
- In this lecture we review DFI, and describe how the method is applied in operational NWP.

The concept of filtering has a rôle in virtually every field of study, *"from topology to theology, seismology to sociology."* 

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It may be represented by a simple system diagram, having an input with both desired and undesired components, and an output comprising only the former.

$$Good/Bad/Ugly \implies Filter \longrightarrow Good$$

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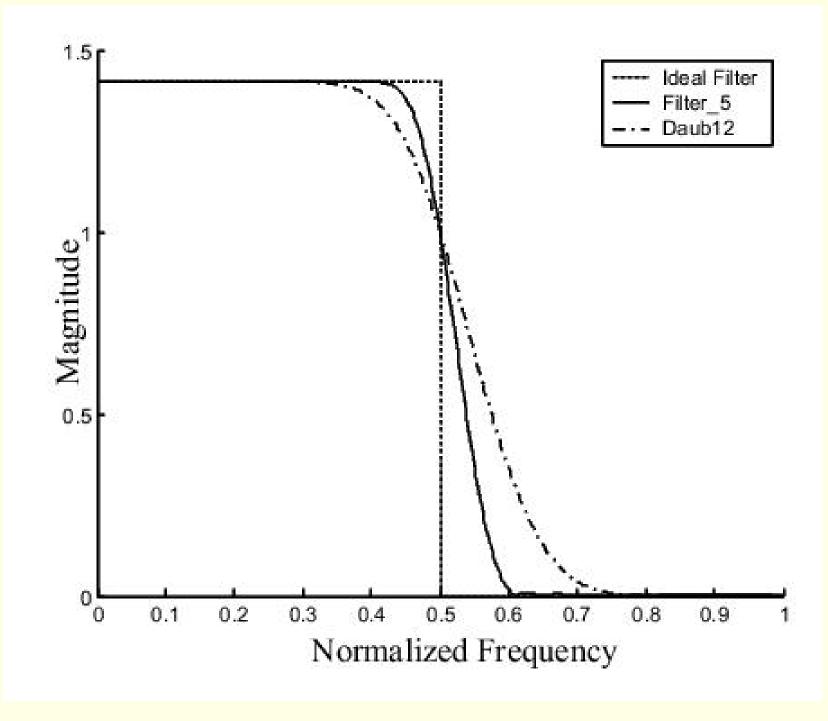
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\* \* \*

Other ideal filters can be discussed:

- High-pass filters
- Band-pass filters
- Notch filters

But the Low-Pass Filter is the one needed for initialization.



Frequency response of ideal low-pass filter.

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To find the frequency response of a recursive filter, let

 $x_n = \exp(in\theta)$ 

and assume an output of the form

 $y_n = H(\theta) \exp(in\theta)$ 

Substitute  $y_n = H(\theta) \exp(in\theta)$  into the defining formula

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For nonrecursive filters the denominator reduces to unity:

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The entire area of filter design is concerned with finding filters haveing desired properties.

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Typically,  $H_c(\omega)$  is a step function

$$H_c(\omega) = \begin{cases} 1, & |\omega| \le |\omega_c|; \\ 0, & |\omega| > |\omega_c|, \end{cases}$$

where  $\omega_c$  is a cutoff frequency.

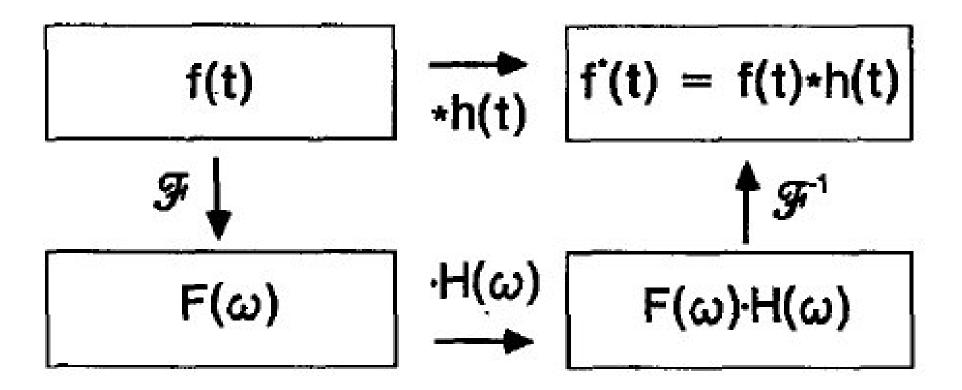


FIG. 1. Schematic representation of the equivalence between convolution and filtering in Fourier space.

Equivalence of filtering and convolution.

$$(h*f)(t) = \mathcal{F}^{-1}\big\{\mathcal{F}\{h\} \cdot \mathcal{F}\{f\}\big\}$$

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For example,  $f_n$  could be the value of some model variable at a particular grid point at time  $t_n$ .

The sequence  $\{f_n\}$  may be regarded as the Fourier coefficients of a function  $F(\theta)$ :

$$F(\theta) = \sum_{n = -\infty}^{\infty} f_n e^{-in\theta},$$

where  $\theta = \omega \Delta t$  is the digital frequency and  $F(\theta)$  is periodic with period  $2\pi$ :  $F(\theta) = F(\theta + 2\pi)$ . [Note:  $\theta_{Ny} = \omega_{Ny} \Delta t = \pi$ ]

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The cutoff frequency  $\theta_c = \omega_c \Delta t$  is assumed to fall in the Nyquist range  $(-\pi, \pi)$  and  $H_d(\theta)$  has period  $2\pi$ .

$$H_d(\theta) = \sum_{n=-\infty}^{\infty} h_n e^{-in\theta} \qquad ; \qquad h_n = \frac{1}{2\pi} \int_{-\pi}^{\pi} H_d(\theta) e^{in\theta} d\theta.$$

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Let  $\{f_n^{\star}\}$  denote the low frequency part of  $\{f_n\}$ , with all components having frequency greater than  $\theta_c$  removed. Clearly,

$$H_d(\theta) \cdot F(\theta) = \sum_{n = -\infty}^{\infty} f_n^{\star} e^{-in\theta}.$$

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We see that the finite approximation to the discrete convolution is identical to a nonrecursive digital filter.

### Gibbs oscillations

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These may be greatly reduced by means of an appropriately defined "window" function.

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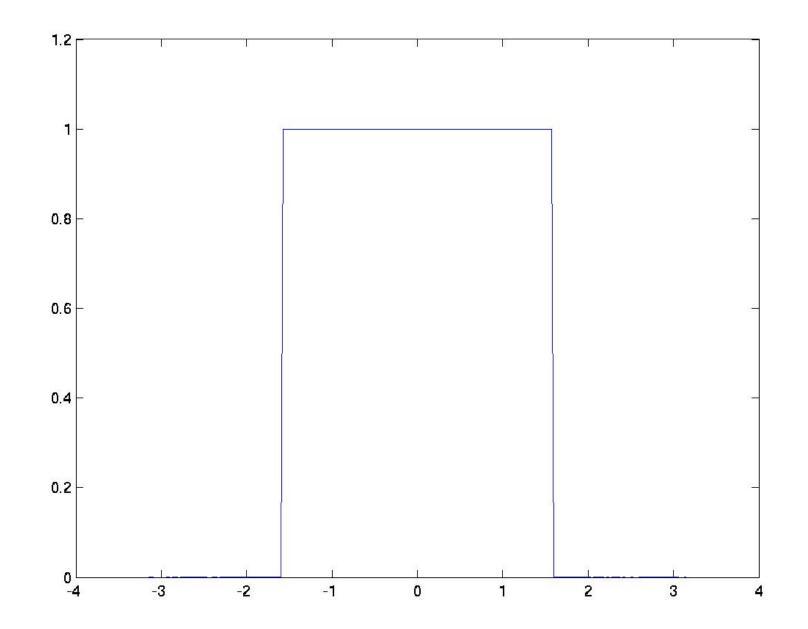
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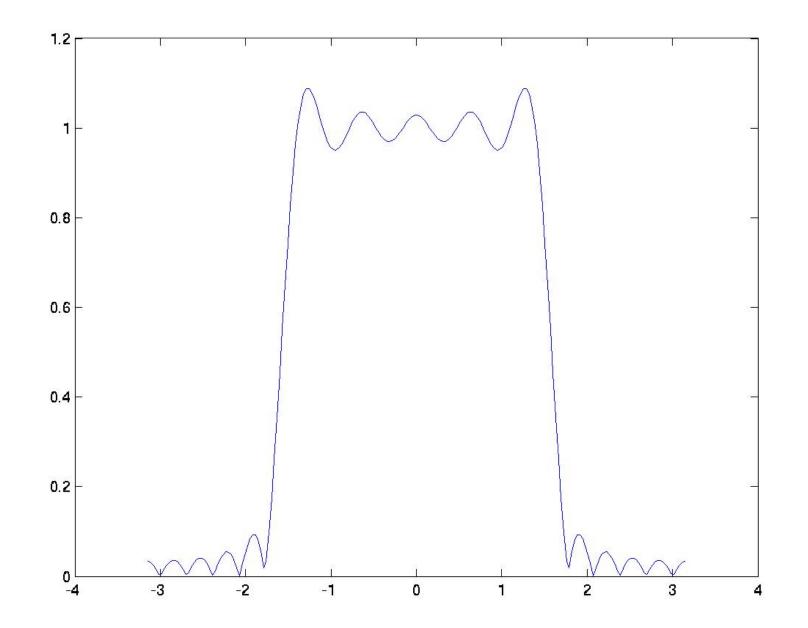
**Exercise:** Write a MATLAB program to compute the FFT of a step function with various truncations. Thus investigate the Gibbs phenomenon.

The truncated Fourier analysis of a square wave is shown in the following figures.

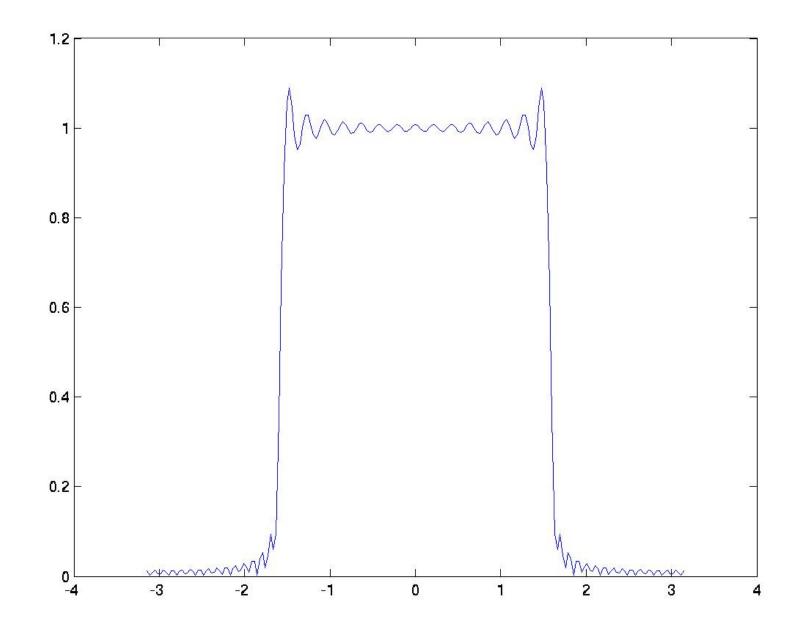
\* \* \*



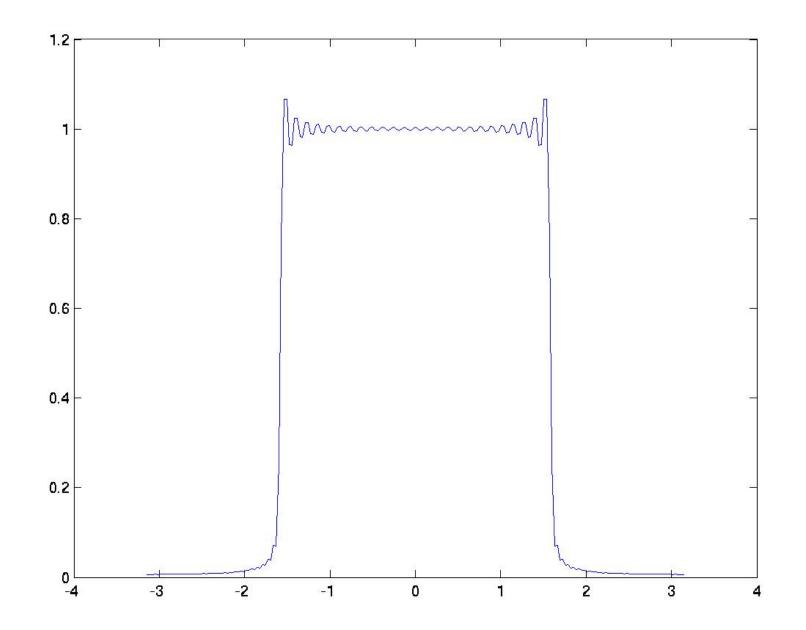
**Original Square wave function.** 



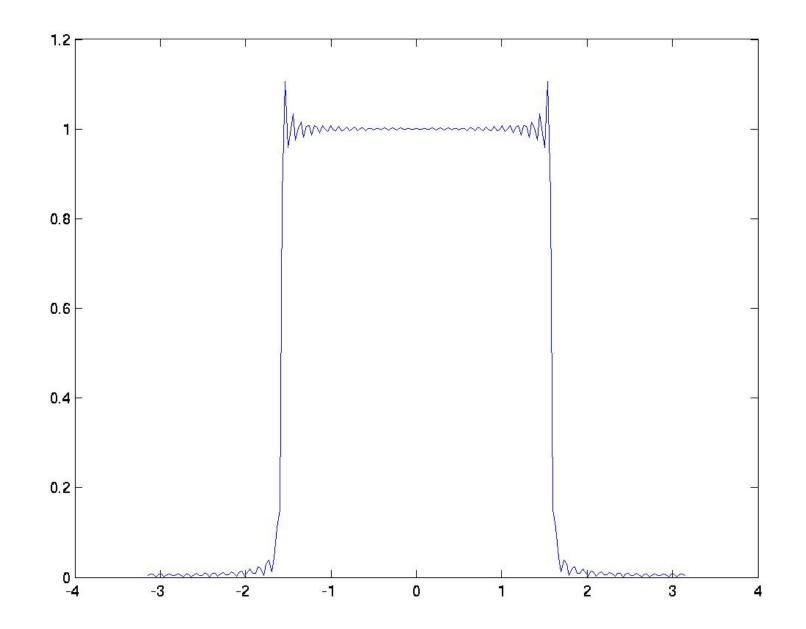
**Truncation:**  $N = 11 (N_{\text{max}} = 50)$ 



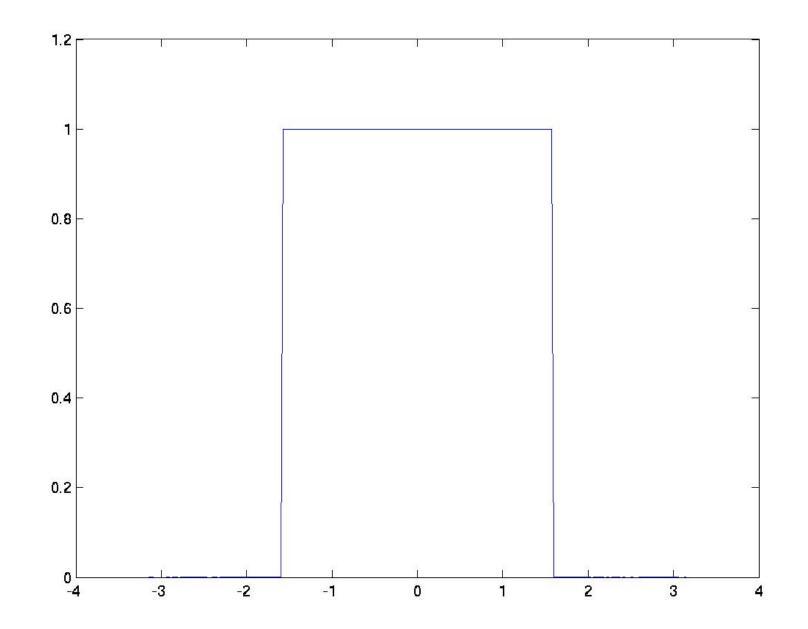
**Truncation:**  $N = 21 (N_{\text{max}} = 50)$ 



**Truncation:**  $N = 31 (N_{\text{max}} = 50)$ 



**Truncation:**  $N = 41 (N_{\text{max}} = 50)$ 



**Original Square wave function.** 

### Application of FIR to Initialization

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With the time step  $\Delta t = 6$  minutes, this corresponds to a (digital) cutoff frequency  $\theta_c = \pi/30$ .

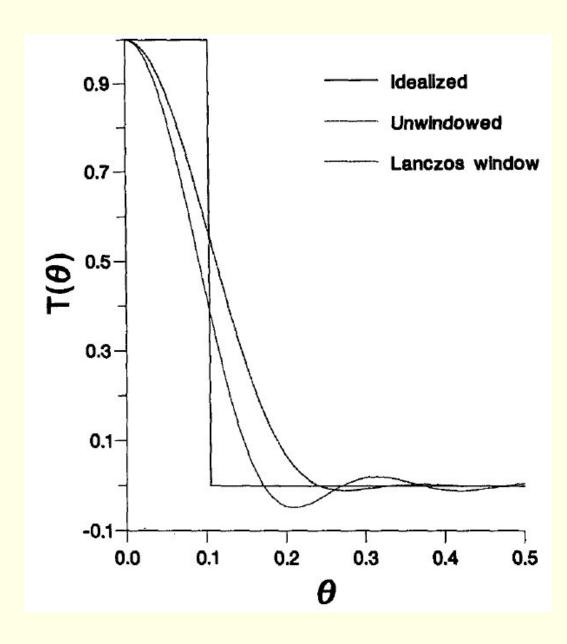
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The coefficients were derived by Fourier expansion of a stepfunction, truncated at N = 30, with a Lanczos window:

$$h_n = \left[\frac{\sin(n\pi/(N+1))}{n\pi/(N+1)}\right] \left(\frac{\sin(n\theta_c)}{n\pi}\right)$$



The use of the window decreases the Gibbs oscillations in the stop-band  $|\theta| > |\theta_c|$ .

However, it also has the effect of widening the pass-band beyond the nominal cutoff.

For a fuller discussion of windowing see *e.g.* Hamming (1989) or Oppenheim and Schafer (1989).

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The uninitialized fields of surface pressure, temperature, humidity and winds were first integrated forward for three hours, and running sums of the form

$$f_F^{\star}(0) = \frac{1}{2}h_0 f_0 + \sum_{n=1}^N h_{-n} f_n,$$

where  $f_n = f(n\Delta t)$ , were calculated for each field at each gridpoint and on each model level.

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These were stored at the end of the three hour forecast.

**Repeat:** 

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These fields correspond to the application of the digital filter to the original data. They are the filtered data.

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Ideally, <u>the phase-error should be as small as possible</u> for the low frequency components which are meteorologically important.

It is salutary to recall that phase-errors are amongst the most prevalent and pernicious problems in forecasting. Break here

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We give here the definition and principal properties of the Dolph-Chebyshev filter.

For further information, see Lynch, 1997 (http://maths.ucd.ie/~plynch).

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In the interval  $|x| \leq 1$ ,  $T_n(x)$  oscillates between +1 and -1.

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By means of the definition of  $T_n(x)$  and basic trigonometric identities,  $H(\theta)$  can be written as a finite expansion

$$H(\theta) = \sum_{n=-M}^{+M} h_n \exp(-in\theta).$$

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The coefficients  $\{h_n\}$  may be evaluated from the inverse Fourier transform

$$h_n = \frac{1}{N} \left[ 1 + 2r \sum_{m=1}^M T_{2M} \left( x_0 \cos \frac{\theta_m}{2} \right) \cos m\theta_n \right] ,$$

where  $|n| \leq M$ , N = 2M + 1 and  $\theta_m = 2\pi m/N$ .

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The weights  $\{h_n : -M \le n \le +M\}$  define the Dolph-Chebyshev or, for short, Dolph filter.

The desired frequency cut-off is specified by choosing a value for the cut-off period,  $\tau_s$ .

Then  $\theta_s = 2\pi \Delta t / \tau_s$  and the parameters  $x_0$  and r are given by

$$\frac{1}{x_0} = \cos\frac{\theta_s}{2}, \quad \frac{1}{r} = \cosh\left(2M\cosh^{-1}x_0\right)$$

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The Dolph filter has minimum ripple-ratio for a given mainlobe width and filter order.

Suppose components with period less than three hours are to be eliminated ( $\tau_s = 3$  h) and the time step is  $\Delta t = \frac{1}{8}$  h.

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The parameters chosen for the DFI are:

- Span  $T_{\rm S} = 2 \,\mathrm{h}$
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So, M = 8, N = 17 and  $\theta_s = 2\pi \Delta t / \tau_s \approx 0.26$ .

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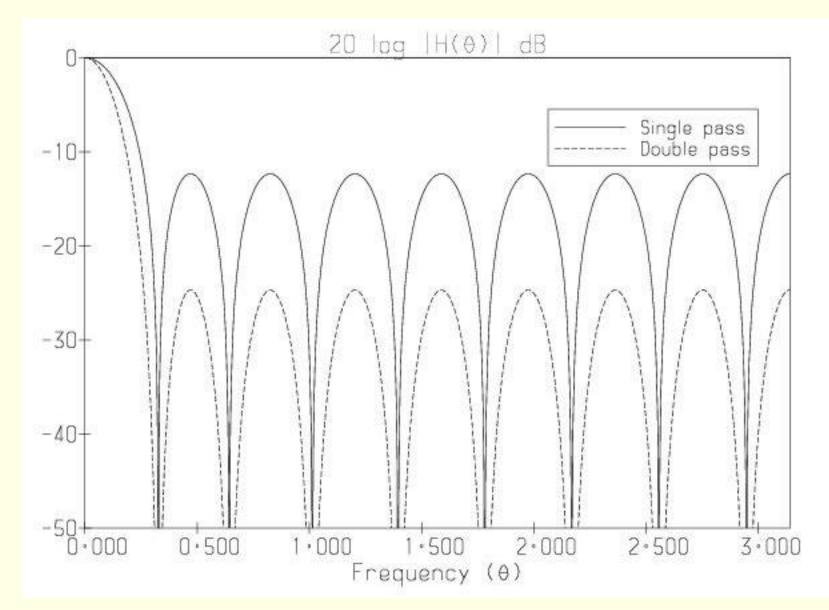
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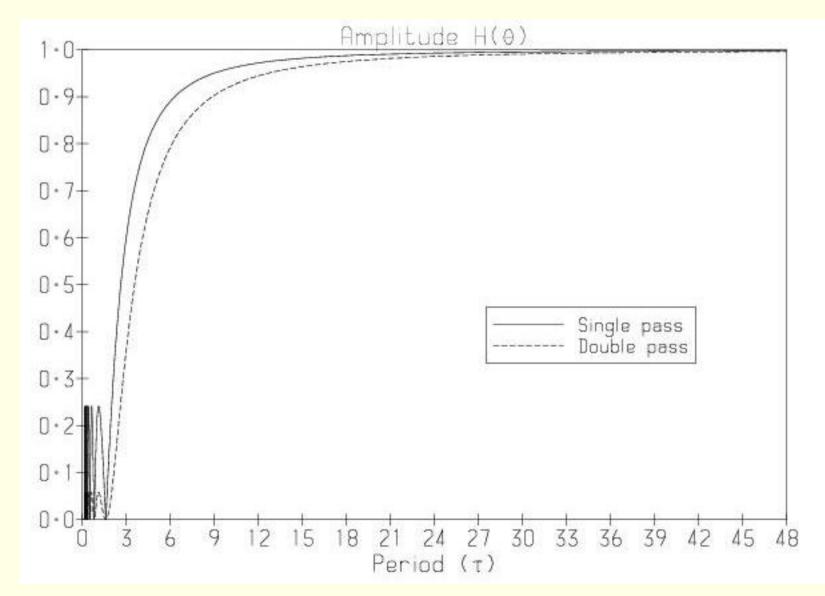
So, M = 8, N = 17 and  $\theta_s = 2\pi \Delta t / \tau_s \approx 0.26$ .

The DFI procedure employed in the HIRLAM model involves a double application of the filter.

We examine the frequency response  $H(\theta)$  and its square,  $H(\theta)^2$  (a second pass squares the frequency response).



Frequency response for Dolph filter with span  $T_S = 2h$ , order N = 2M + 1 = 17 and cut-off  $\tau_s = 3h$ . Results for single and double application are shown. Logarithmic response (dB) as a function of frequency.



Frequency response for Dolph filter with span  $T_S = 2h$ , order N = 2M + 1 = 17 and cut-off  $\tau_s = 3h$ . Results for single and double application are shown. Amplitude response as a function of period.

A single pass attenuates high frequencies (components with  $|\theta| > |\theta_s|$ ) by at least 12.4dB.

For a double pass, the minimum attenuation is about 25dB, more than adequate for elimination of HF noise.

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It can be proved (Lynch, 1997) that the Dolph window is an optimal filter whose pass-band edge,  $\theta_p$ , is the solution of the equation  $H(\theta) = 1 - r$ .

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The filter output is calculated by accumulating the sums

$$\bar{x} = \sum_{n=0}^{n=-N} h_{N-n} x_n \,.$$

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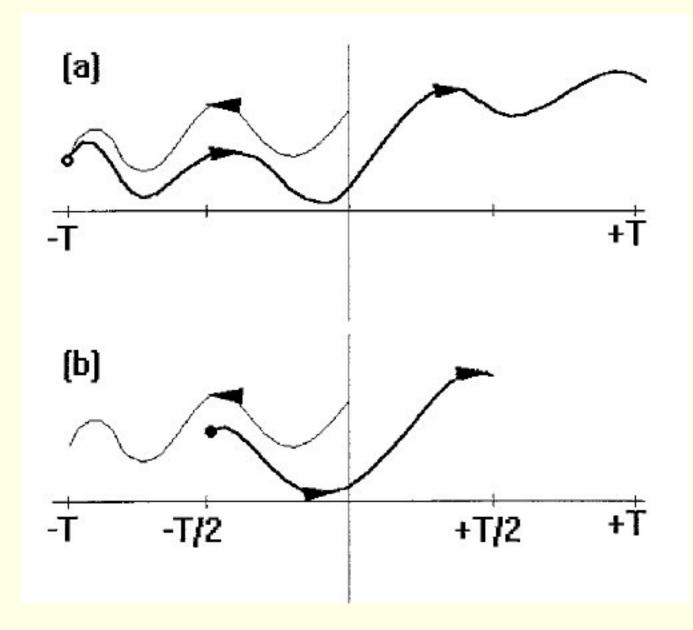
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Again, the filter is applied by accumulating sums formally identical to those of the first stage.

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The output of the second pass is the initialized data.



### **DFI: Sample Results**

The basic measure of noise is the mean absolute value of the surface pressure tendency

$$N_1 = \left(\frac{1}{\text{NGRID}}\right) \sum_{n=1}^{\text{NGRID}} \left|\frac{\partial p_s}{\partial t}\right|$$

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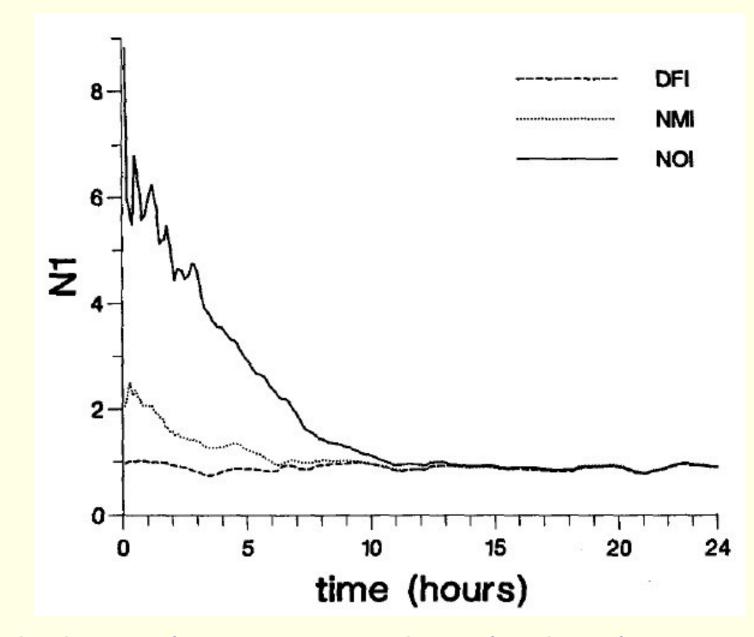
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For uninitialized fields it can be up to an order of magnitude larger.

In the following figure, we plot the value of  $N_1$  for three forecasts.



Mean absolute surface pressure tendency for three forecasts. Forecast with no initialization (NIL); normal mode initialization (NMI); digital filter initialization (DFI). Units are hPa/3 hours. The measure  $N_1$  indicates the noise in the vertically integrated divergence field.

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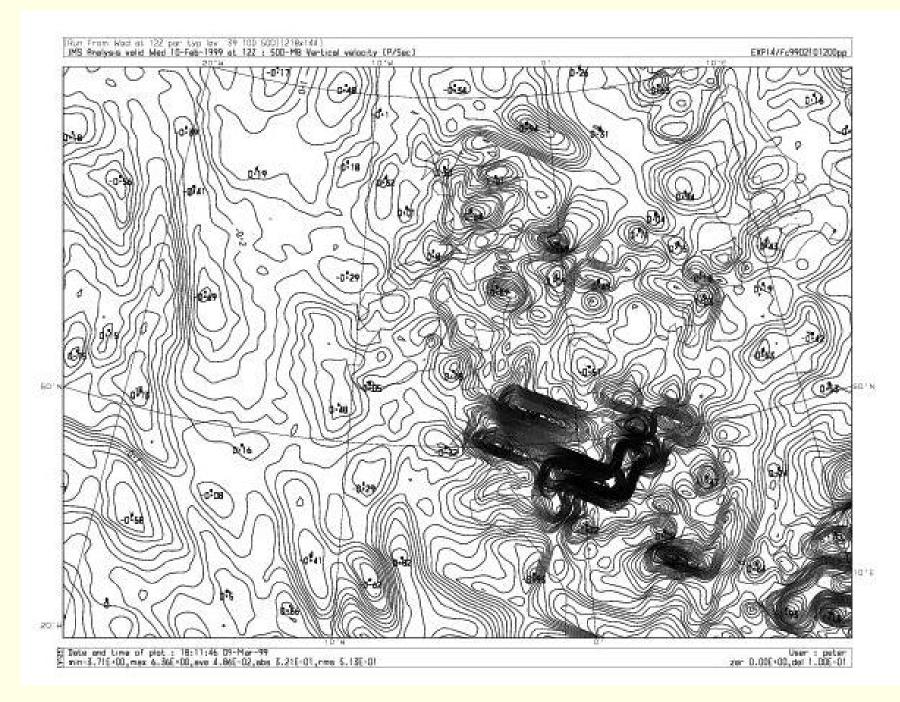
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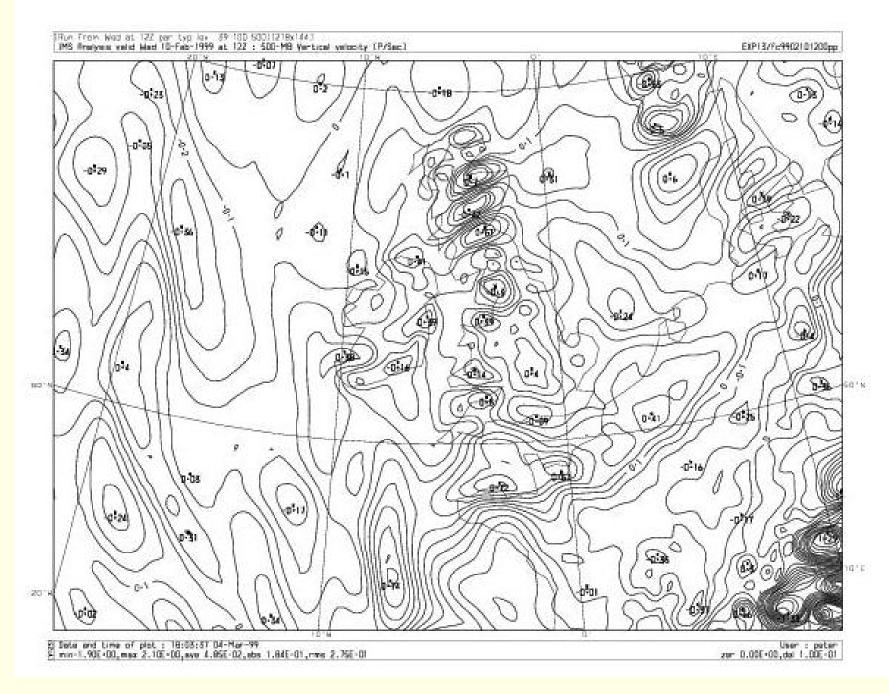
\* \* \*

The uninitialized vertical velocity field is physically quite unrealistic.

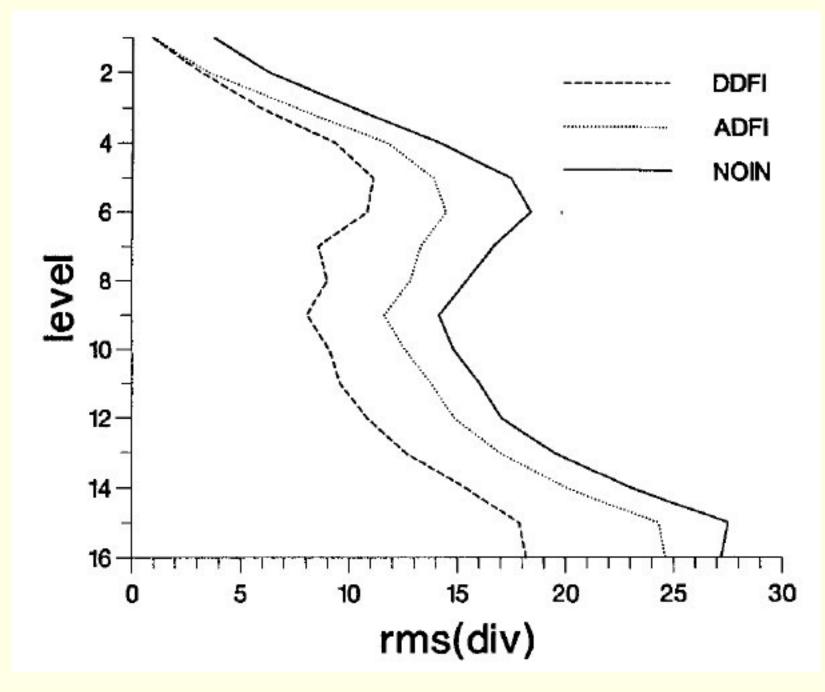
The DFI vertical velocity is much smoother, and much more realistic.



Vertical velocity at 500 hPa for uninitialized analysis (NIL).



Vertical velocity at 500 hPa after digital filtering (DFI).



Root mean square divergence at each model level.

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End of §4.3