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Thus, the mean of a product has two components:

$$\overline{w\theta} = \overline{(\overline{w} + w')(\overline{\theta} + \theta')} \\
= \overline{(\overline{w}\overline{\theta} + \overline{w}\theta' + w'\overline{\theta} + w'\theta')} \\
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$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z} = 0$$

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The total time derivative of u is

$$\frac{du}{dt} = \frac{\partial u}{\partial t} + u\frac{\partial u}{\partial x} + v\frac{\partial u}{\partial y} + w\frac{\partial u}{\partial z} + u\left(\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z}\right)$$
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Writing sums of mean and eddy parts and averaging:

$$\overline{\frac{du}{dt}} = \frac{\partial \overline{u}}{\partial t} + \frac{\partial}{\partial x} \left( \overline{u} \,\overline{u} + \overline{u'u'} \right) + \frac{\partial}{\partial y} \left( \overline{u} \,\overline{v} + \overline{u'v'} \right) + \frac{\partial}{\partial z} \left( \overline{u} \,\overline{w} + \overline{u'w'} \right)$$

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But the mean flow is nondivergent, so

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$$\frac{du}{dt} = \frac{\partial \overline{u}}{\partial t} + \frac{\partial}{\partial x} \left( \overline{u'u'} \right) + \frac{\partial}{\partial y} \left( \overline{u'v'} \right) + \frac{\partial}{\partial z} \left( \overline{u'w'} \right)$$

$$\frac{\overline{d}\overline{u}}{dt} - f\overline{v} + \frac{1}{\rho_0}\frac{\partial\overline{p}}{\partial x} + \left[\frac{\partial}{\partial x}\left(\overline{u'u'}\right) + \frac{\partial}{\partial y}\left(\overline{v'u'}\right) + \frac{\partial}{\partial z}\left(\overline{w'u'}\right)\right] = 0$$

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The thermodynamic equation may be expressed in a similar way:

$$\frac{\overline{d}\,\overline{\theta}}{dt} + \overline{w}\frac{d\theta_0}{dz} + \left[\frac{\partial}{\partial x}\left(\overline{u'\theta'}\right) + \frac{\partial}{\partial y}\left(\overline{v'\theta'}\right) + \frac{\partial}{\partial z}\left(\overline{w'\theta'}\right)\right] = 0$$

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The terms in square brackets are the *turbulent fluxes*.

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In the free atmosphere, the terms in square brackets are sufficiently small that they can be neglected.

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Within the boundary layer, the turbulent flux terms are comparable in magnitude to the remaining terms, and must be included in the analysis. In the boundary layer, vertical gradients are generally orders of magnitude larger than variations in the horizontal. Thus, it is possible to omit the x and y derivative terms in the square brackets. In the boundary layer, vertical gradients are generally orders of magnitude larger than variations in the horizontal. Thus, it is possible to omit the x and y derivative terms in the square brackets.

Then the complete system of equations becomes

$$\frac{d\overline{u}}{dt} - f\overline{v} + \frac{1}{\rho_0}\frac{\partial\overline{p}}{\partial x} + \frac{\partial}{\partial z}\left(\overline{w'u'}\right) = 0$$

$$\frac{d\overline{v}}{d\overline{v}} + f\overline{u} + \frac{1}{\rho_0}\frac{\partial\overline{p}}{\partial y} + \frac{\partial}{\partial z}\left(\overline{w'v'}\right) = 0$$

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Next, we will consider a simple parameterization of the vertical momentum flux,  $\partial(\overline{w'u'})/\partial z$ .

#### The momentum equations will be taken in the form

$$\frac{du}{dt} - fv + \frac{1}{\rho_0} \frac{\partial p}{\partial x} + \frac{\partial}{\partial z} \left( \overline{w'u'} \right) = 0$$
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In the free atmosphere, scale analysis shows that the inertial terms and turbulent flux terms are small compared to the Coriolis term and pressure gradient terms.

This leads us to the relation for geostrophic balance:

$$u \approx u_G \equiv -\frac{1}{f\rho_0} \frac{\partial p}{\partial y}, \qquad v \approx v_G \equiv +\frac{1}{f\rho_0} \frac{\partial p}{\partial x}$$

In the boundary layer, it is no longer appropriate to neglect the turbulent flux terms. However, the inertial terms may still be assumed to be relatively small. In the boundary layer, it is no longer appropriate to neglect the turbulent flux terms. However, the inertial terms may still be assumed to be relatively small.

Thus we get a three-way balance between the forces:

$$-fv + \frac{1}{\rho_0}\frac{\partial p}{\partial x} + \frac{\partial}{\partial z}\left(\overline{w'u'}\right) = 0$$
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$$-f(v - v_G) + \frac{\partial}{\partial z} \left( \overline{w'u'} \right) = 0$$
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To progress, we need some means of representing the turbulent fluxes in terms of the mean variables.

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Thus, the flux of momentum is assumed to be proportional to the vertical gradient of the mean momentum. Then we can write

$$\overline{u'w'} = -K\left(\frac{\partial\overline{u}}{\partial z}\right)$$

where K is called the *eddy viscosity coefficient*.

This closure scheme is often referred to as K-theory. Alternatively, we may call it the Flux-gradient theory.

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We will assume that K is constant. Thus, for example,

$$\frac{\partial}{\partial z} \left( \overline{w'u'} \right) = -\frac{\partial}{\partial z} \left( K \frac{\partial u}{\partial z} \right) = -K \frac{\partial^2 u}{\partial z^2}$$

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The momentum equations then become

$$-f(v - v_G) - K\frac{\partial^2 u}{\partial z^2} = 0$$
$$+f(u - u_G) - K\frac{\partial^2 v}{\partial z^2} = 0$$

In the following lecture, we will use these equations to model the Ekman Layer.

#### End of §5.3